

Detection of hexavalent uranium with inline and field-portable immunosensors

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Abstract. An antibody that recognizes a chelated form of hexavalent uranium was used in the development of two different immunosensors for uranium detection. Specifically, these sensors were utilized for the analysis of groundwater samples collected during a 2007 field study of *in situ* bioremediation in a aquifer located at Rifle, CO. The antibody-based sensors provided data comparable to that obtained using Kinetic Phosphorescence Analysis (KPA). Thus, these novel instruments and associated reagents should provide field researchers and resource managers with valuable new tools for on-site data acquisition.

Introduction

The ability to perform quantitative analyses of contaminants in groundwater samples while still in the field has been a long-term goal for environmental scientists. For uranium analysis, samples must be transported off-site for any complex, detailed analysis such as ICP-MS or AAS. Simpler instrumentation like the Kinetic Phosphorescence Analyzer (KPA) is also used primarily in a laboratory setting; in addition, this instrument is useful only for the analysis of uranium and lanthanides (Brina and Miller, 1993). Here we describe two immunosensors that can be adapted for uranium analysis through the use of antibodies that bind to a UO_2^{2+} -chelate complex.

Immunoassays have numerous advantages for quantifying levels of environmental contaminants. Immunoassay methods are rapid and simple to perform. Relatively compact instruments can be designed to quantify antibody binding; such instruments are thus amenable for use in a field setting. Finally, the immunosensors used in the experiments described herein can be modularized such that many different contaminants can be measured using an identical sensor plat-

form; if an antibody to a specific environmental contaminant can be generated, it can be used with this sensor technology. In the present study, two instruments based on the principle of kinetic exclusion (Blake 1999, Kusterbeck and Blake 2008) were used to assay groundwater samples from a uranium-contaminated site in Rifle, CO. Both immunosensors were able to detect changes in uranium levels during an *in situ* remediation process and thus show promise towards eventual field deployment for a variety of environmental sensing needs.

Methods

Materials

The uranium-selective chelator 2,9-dicarboxyl-1,10-phenanthroline (DCP) was purchased from Alfa Aesar (Ward Hill, MA). 12F6, a mouse monoclonal antibody that binds specifically a UO_2^{2+} -DCP complex, and an immobilized form of chelated uranium (UO_2^{2+} -DCP-BSA conjugate) were available from a previous study (Blake et al. 2004). A Cy5-labeled Fab of goat anti-mouse IgG was obtained from Jackson ImmunoResearch Laboratories (Gaithersburg, MD). Bisacrylamide/azlactone copolymer beads (UltraLink Biosupport), used in the Inline sensor, were a product of Pierce Biotechnology (Rockford, IL). Polystyrene beads, used with the field portable device (FPD), were acquired from Sapidyne Instruments, Inc (Boise, ID). The diameter of both bead types was $\sim 98 \mu\text{m}$; these beads were coated with the UO_2^{2+} -DCP-BSA conjugate by procedures that have been previously described (Blake et al, 2004; Yu et al, 2005). A UO_2^{2+} standard was made from uranyl acetate obtained from Mallinckrodt (St. Louis, MO). Environmental water samples were obtained in August and September, 2007 from a sampling well (D-02) at the Rifle UMTRA site, Rifle CO. The collected samples (~ 50 ml each) were filtered through a $0.2 \mu\text{M}$ IC MILLEX-LG syringe filter (Millipore, Billerica, MA) and refrigerated. All samples were acidified with 8 N HNO_3 to a pH of 2 before analysis. Standard curves were generated using a 1:200 dilution of "Rifle Artificial Ground Water" (RAGW), made from a formulation developed by K.M. Campbell of the U.S. Geological Survey (Menlo Park, CA).

Inline Sensor

The Inline sensor, developed in conjunction with Sapidyne Instruments (Boise, ID) (Fig. 1A) is an instrument designed to be operated in a process line capacity (Yu et al., 2005; Bromage et al., 2007; Kusterbeck and Blake, 2008).

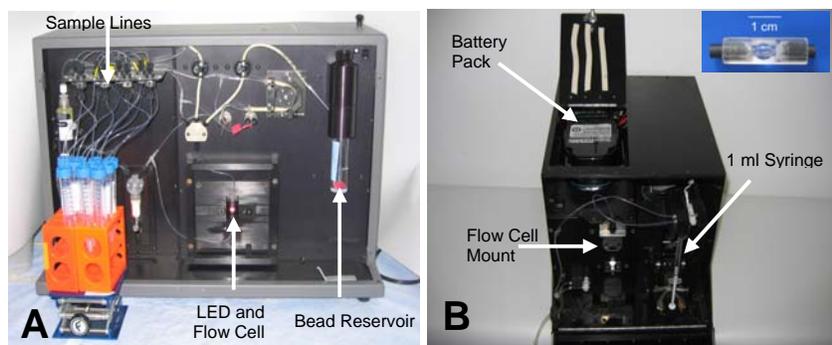


Fig 1 Uranium immunosensors. **A**, The KinExA Inline sensor (footprint, 30x56 cm) autonomously mixes assay components and injects them over a capillary bead column illuminated by an LED. The instrument measures fluorescently labeled antibody bound to the column; multiple samples can be assayed in one experimental run. **B**, The Field Portable Device (footprint, 23.5 x 32 cm) is a self-contained instrument that injects operator-prepared samples from a loaded 1 ml syringe over a pre-filled flow cell (**inset**). The instrument with battery weighs approximately 6 kilograms; a carrying case with room for all necessary accessories (not shown) increases portability.

The Inline sensor required a grounded power source and was able to autonomously mix all components, run a standard curve, and analyze unknowns. Bis-acrylamide/azlactone copolymer beads (50 mg) were coated with UO_2^{2+} -DCP-BSA conjugate and loaded into the bead reservoir before the assay sequence was initiated. UO_2^{2+} was spiked into HEPES-buffered saline (HBS, 137 mM NaCl, 3 mM KCl, 10 mM HEPES, pH 7.4) containing 200 nM DCP and a 1:200 dilution of RAGW in order to generate the standard curve. Environmental samples were diluted 1:200 in HEPES-buffered saline containing 200 nM DCP. The pH of the environmental samples after a 1:200 dilution into HBS was between 7.0 and 7.2. All assay mixtures also contained the anti-uranium antibody 12F6 (0.25 nM) and Cy5-Fab (5 nM, used to fluorescently label 12F6). The signals generated by the environmental samples were compared to the standard curve to determine concentrations of UO_2^{2+} . The instrument was programmed (Yu et al, 2005) to generate a five-point standard curve and analyze seven samples in a single experimental run. All data points (standards and environmental samples) were obtained in triplicate.

Field Portable Device

The field portable device (FPD) (Fig. 1B), also developed in conjunction with Sapidyne Instruments (Kusterbeck and Blake, 2008), was designed to be used in the field without the need for a grounded power supply. Instead, the device was powered with a power drill battery available at most hardware stores. The instru-

ment was completely enclosed in a plastic case and controlled by laptop through a wireless interface. Unlike the re-usable capillary flow cell utilized by other kinetic exclusion instruments (Blake et al., 2004; Yu et al., 2005), the FPD used a disposable flow cell (Fig. 1B, inset) prefilled with polystyrene beads coated with the UO_2^{2+} -DCP-BSA conjugate. Assay components were mixed by the operator; the final concentrations of the reagents were as described for Inline sensor analysis, except the Cy5-Fab concentration was reduced to 2.5 nM. Due to the limited binding capacity of the flow cell, the data points of the standard curve were obtained in singlet, while the environmental sample was analyzed in triplicate.

Kinetic Phosphorescence Analysis

In order to validate the performance of the immunosensors described herein, acidified groundwater samples were also analyzed with a kinetic phosphorescence analyzer (KPA) and Uraplex reagent available from ChemCheck Instruments (Bellevue, WA). Each sample was measured at three dilutions to ensure accuracy.

Results

The Inline sensor and the FPD are both flow fluorimeters that employ the kinetic exclusion method. This method measures the concentration of free, uncomplexed antibody in assay mixtures containing fluorescently-labeled antibody, the contaminant of interest, and antibody-contaminant complexes (Blake et al, 1999). A structural analogue of the contaminant (in this case chelated uranium) was coated onto beads. These beads were subsequently packed into a flow cell and used to capture the free fluorescently-labeled antibody; the fluorescence on the beads was monitored as the assay mixture flowed through the cell.

Typical data traces for the FDP are shown in Fig 2. This instrument recorded the baseline fluorescence 5 seconds prior to injection of the sample. Sample injection was completed in ~50 seconds and the instrument then automatically rinsed the flow cell from a buffer reservoir. The instrument automatically determined the baseline signal from the first 5 seconds of the trace and subtracted that value from the final signal after the rinse to generate a “delta” signal, which was inversely proportional to the amount of UO_2^{2+} in the sample. A delta signal for each sample could be determined in 140 seconds.

In order to generate a standard curve, known amounts of UO_2^{2+} were added to a buffered sample that contained 200 nM DCP chelator and RAGW in the same dilution as that used for the environmental samples. The chelated UO_2^{2+} bound to fluorescently labeled 12F6 antibodies present in the sample; these bound antibodies were therefore not available for binding to the chelated UO_2^{2+} immobilized on the beads. As more soluble UO_2^{2+} was added to the assays, less fluorescently labeled antibody was bound to the beads. This competition for limited antibody

binding sites resulted in a delta signal from the instrument that was inversely proportional to the amount of UO_2^{2+} present in the sample.

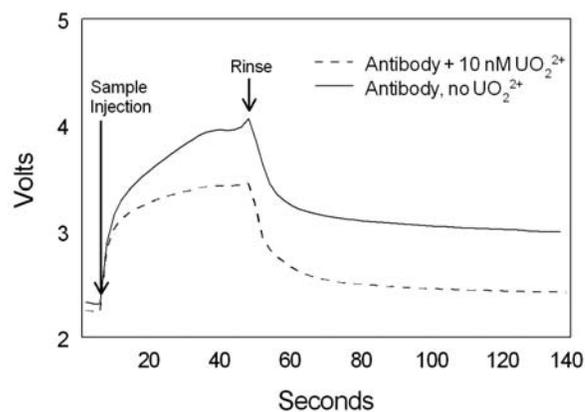


Fig 2. Primary data traces from the FPD. Solid line, sample containing antibody but no UO_2^{2+} . Dashed line, sample containing antibody plus a UO_2^{2+} concentration high enough to fill all antibody binding sites (10 nM).

A 4-point standard curve was generated using the FPD, as shown in Fig 3.

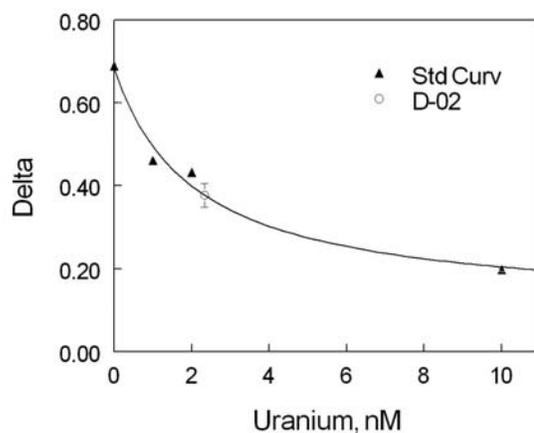


Fig 3. Uranium standard curve developed using the FPD. UO_2^{2+} standards (closed triangles) and a sample from a sampling well in Rifle (well D-02, open circle) were prepared as described in Methods. The concentration of UO_2^{2+} present in the sample after factoring in the dilution was 473.1 ± 87.9 nM. Points obtained for generation of the standard curve were singlets while the environmental sample was run in triplicate.

The standard curves were fit to the data points using the following equation:

$$Y_A = \frac{a0 - (a1 * x)}{a2 + x} \quad (\text{Eq 1})$$

in which Y_A is the delta value at a particular concentration of UO_2^{2+} , $a0$ is the delta at an infinite concentration, $a1$ is the magnitude of change in delta from the lowest to the highest UO_2^{2+} concentrations and $a2$ is the concentration of UO_2^{2+} that results in 50% inhibition of the signal. The $a2$ is also the equilibrium dissociation constant (K_d) of 12F6 binding to the UO_2^{2+} -DCP complex. Since this value has been determined in a previous study (Blake et al., 2004), the $a2$ obtained was a reliable indicator of the accuracy of the standard curve. The amount of UO_2^{2+} in an environmental sample was determined by diluting the environmental sample into HBS buffer containing the same reagents used for the standard curve. The sample was then injected over the beads and the resultant data point was fitted onto the standard curve.

Similar analyses were also performed using the Inline sensor. In contrast to the FPD, which used a single bead pack in a disposable flow cell for multiple measurements, the Inline sensor used a fresh set of beads for each measurement. Beads were stored as a slurry in a reservoir bottle (shown in Fig 1A) and the instrument automatically packed a new bead microcolumn at the beginning of each measurement. Typical data traces from the Inline sensor are shown in Fig. 4. The *inset* shows a uranium standard curve prepared by plotting delta versus uranium concentration.

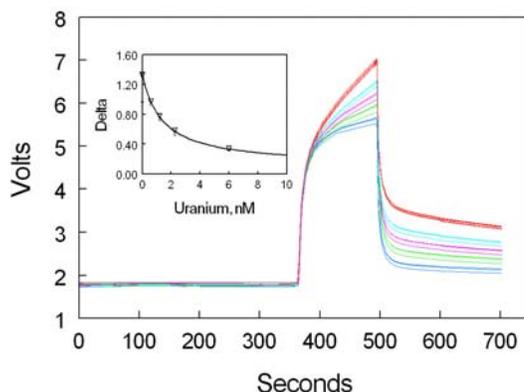


Fig 4. Data traces and uranium standard curve from the Inline sensor. The instrument packed beads into the flow cell, washed sample lines and tubes and mixed experimental samples from stock solutions from 0-359 sec. Sample injection occurred at 360 seconds and was followed by a buffer rinse. *Inset*, Uranium standard curve. All experiments were performed in triplicate.

Finally, both the FPD and the Inline sensor were compared with kinetic phosphorescence analysis for their ability to assess uranium in environmental groundwater samples. These samples were obtained during an *in situ* bioremediation experiment conducted at the Uranium Mill Tailings Remedial Action (UMTRA) site located in Rifle, CO. Detailed descriptions of the history, geology and hydrogeology of this site have been described elsewhere (Anderson, et al., 2003; Vrionis, et al., 2005). Background groundwater concentrations of uranium are approximately 500 to 1000 nM. A series of monitoring wells were installed down-gradient of an injection gallery. This injection gallery, installed perpendicular to the groundwater flow, was used to pump acetate into the aquifer. Biostimulation with acetate is thought to initially stimulate the growth of *Geobacter* species, which are able to reduce soluble U(VI) to insoluble U(IV) and decrease the uranium in the water column (N'Guessan et al., 2008). Groundwater samples were collected at intervals after initiation of acetate injection and analyzed for uranium. Fig 5 shows the levels of soluble uranium in a representative downstream well, D-02, during continuous acetate injection from the day 0 to day 35. As reported previously (N'Guessan, 2008) acetate injection caused a relatively sharp decrease in soluble uranium that was detected with all three instruments. Additionally, the data from the two immunosensors correlated well with the data from the KPA.

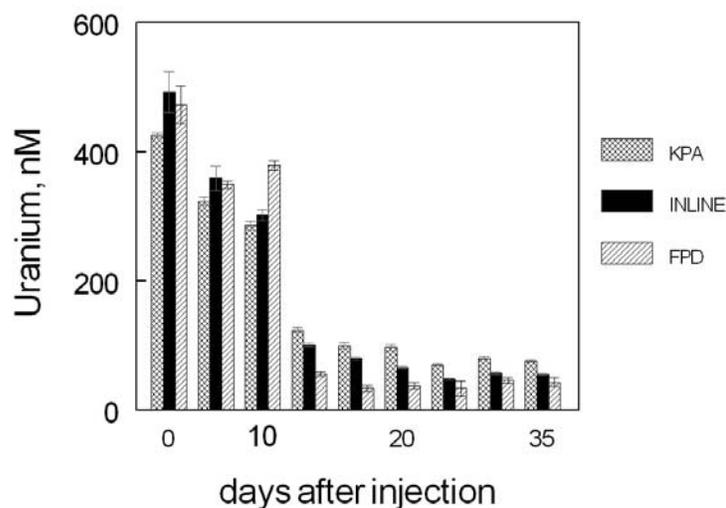


Fig 5. Comparison of KPA, Inline, and FPD analysis. Groundwater samples were collected at the indicated times after the initiation of acetate injection, filtered and acidified. KPA analyses were performed at 3 dilutions; samples were analyzed in triplicate using the Inline Sensor and FPD. The error bars represent the standard error of the mean.

Discussion

Previous work in our laboratory has focused on the isolation/characterization of antibodies that bind to metal-chelate complexes and on the development of antibody-based assays useful for measuring a variety of heavy metals in a given sample (Khosraviani et al., 1998; Delehanty et al., 2003; Darwish and Blake, 2004; Kriegel et al., 2006; Zhu et al., 2007). The work described in this report represents some of the first experiments carried out by our laboratory in a field setting and demonstrates the portability, speed and overall utility of immunosensors for environmental analysis. However, as with all immunoassays, a detailed understanding of the binding properties of the antibody used in the assay is vital for the success of this method.

Monoclonal antibodies that recognize environmental contaminants are typically generated in mice by repeated exposure of the contaminant (or a structural analogue of the contaminant) to the mouse immune system. Metal cations are too small to illicit an immune response and our laboratory has developed a method whereby an immunogen is prepared by immobilizing the metal via a bifunctional chelator to a carrier protein (for a review, see Blake et al., 2007). The antibodies generated from such immunizations recognize metals bound to a chelator, rather than free metals. Since metals in environmental samples almost always exist in a complexed state, an important part of any assay development effort is devising a strategy that removes the metal from its natural complexants and transforms it to a form recognized by the antibody. The antibody used for the uranium analysis, 12F6, recognizes uranium in a complex with DCP (Blake et al, 2004). Thus, the uranium in the environmental samples from the Rifle site had to be dissociated from complexants present in the groundwater samples and subsequently transformed to DCP complexes. While the optimal pre-treatment strategy for Rifle samples (acidification, then neutralization into buffers containing DCP) was not determined until after the field experiment had been completed, future experiments should allow for near real-time quantification of uranium in the field.

The use of the Inline sensor has both advantages and disadvantages for field use. This instrument had a relatively high sample throughput and provided data with minimal effort on the part of the operator. In a typical day at Rifle, we collected and pretreated samples during a day of field work; the Inline sensor was then programmed to analyze them overnight. The instrument's autonomous operation and relatively small footprint (30x56 cm) was advantageous in the cramped conditions that existed in our field laboratory (a converted horse trailer). The Inline sensor provided data that was as precise as larger immunoassay instruments in our laboratory. This superior precision could be attributed to the instrument's ability to prepare a fresh set of reagents (bead column, freshly mixed assay components) for each measurement; however, use of fresh reagents limited the total number of individual samples per run to ~50. The main disadvantage of the Inline sensor was its requirement for a grounded 110 AC power source.

Because of its independent power supply and wireless interface, the FPD could be operated in the absence of a grounded power supply (although the drill

batteries used for operation needed to be recharged either from an automotive battery or a grounded power source). The instrument is comparatively light (6 kg); it was transported in a backpack-like bag that also had room for all necessary reagents and accessories (pipettes, syringes, disposable tubes); thus, this instrument could be used in a remote setting. One of the issues currently being addressed during further FPD development is the binding capacity of the disposable flow cells supplied with the instrument. Unlike the Inline immunosensor, the FPD uses the same bead column for multiple measurements. This ultimately results in a decrease in instrument responsiveness as more and more antibody binds to the UO_2^{2+} -DCP coated on the beads. For the experiments described herein, we responded by limiting the number of standards and experimental samples analyzed on each disposable flow cell. In practical terms, these limitations decreased precision due to fewer replicate measurements. A fresh flow cell was required for every environmental sample, which led to a decrease in sample throughput. New bead coating strategies and sample injection schemes are being explored to optimize instrument performance.

The data obtained with these two new immunosensors compared well that obtained using KPA. As seen in Fig 5, the data from both the Inline and FPD correlated well with the KPA analysis of the D-02 test well, especially at the higher uranium levels seen at the beginning of this study. While the FPD, in particular, was less able to monitor uranium at lower levels, both the Inline sensor and the FPD were able to detect the removal of uranium from the groundwater sample collected during experiments performed during the summer of 2007.

The immunosensors described herein can be easily adapted to the analysis of a wide variety of other experimental contaminants. Assays for other heavy metals, PCB's, 2,4-dichlorophenoxyacetic acid, environmental estrogens, organophosphate pesticides, imidazolinone herbicides and TNT have been published using the KinExA™ technology employed by the Inline sensor and FPD (for a review, see Kusterbeck and Blake, 2008). These new field deployable sensors will provide researchers and resource managers with an invaluable tool for generating near real-time data and modifying field experiments already in progress.

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